

The Shock Absorber Handbook

Second Edition

John C. Dixon, Ph.D, F.I.Mech.E., F.R.Ae.S.

Senior Lecturer in Engineering Mechanics

The Open University, Great Britain



John Wiley & Sons, Ltd



**Professional
Engineering
Publishing**

This Work is a co-publication between Professional Engineering Publishing Ltd and John Wiley and Sons, Ltd.

The Shock Absorber Handbook
Second Edition

Wiley-Professional Engineering Publishing Series

This series of books from John Wiley Ltd and Professional Engineering Publishing Ltd aims to promote scientific and technical texts of exceptional academic quality that have a particular appeal to the professional engineer.

Forthcoming titles:

Vehicle Particulate Emissions

Peter Eastwood

Suspension Analysis and Computational Geometry

John C. Dixon

Managing Reliability Growth in Engineering Design: Decisions, Data and Modelling

Lesley Walls and John Quigley

The Shock Absorber Handbook

Second Edition

John C. Dixon, Ph.D, F.I.Mech.E., F.R.Ae.S.

Senior Lecturer in Engineering Mechanics

The Open University, Great Britain



John Wiley & Sons, Ltd



**Professional
Engineering
Publishing**

This Work is a co-publication between Professional Engineering Publishing Ltd and John Wiley and Sons, Ltd.

This Work is a co-publication between Professional Engineering Publishing Ltd and John Wiley and Sons, Ltd.

Previously published as *The Shock Absorber Handbook, 1st Edition*, by The Society of Automotive Engineers, Inc, 1999, ISBN 0-7680-0050-5.

By the same author: *Tires, Suspension and Handling (SAE)*.

Copyright © 2007 John Wiley & Sons Ltd, The Atrium, Southern Gate, Chichester,
West Sussex PO19 8SQ, England
Telephone (+44) 1243 779777

Email (for orders and customer service enquiries): cs-books@wiley.co.uk
Visit our Home Page on www.wiley.com

All Rights Reserved. No part of this publication may be reproduced, stored in a retrieval system or transmitted in any form or by any means, electronic, mechanical, photocopying, recording, scanning or otherwise, except under the terms of the Copyright, Designs and Patents Act 1988 or under the terms of a licence issued by the Copyright Licensing Agency Ltd, 90 Tottenham Court Road, London W1T 4LP, UK, without the permission in writing of the Publisher. Requests to the Publisher should be addressed to the Permissions Department, John Wiley & Sons Ltd, The Atrium, Southern Gate, Chichester, West Sussex PO19 8SQ, England, or emailed to permreq@wiley.co.uk, or faxed to (+44) 1243 770620.

Designations used by companies to distinguish their products are often claimed as trademarks. All brand names and product names used in this book are trade names, service marks, trademarks or registered trademarks of their respective owners. The Publisher is not associated with any product or vendor mentioned in this book.

This publication is designed to provide accurate and authoritative information in regard to the subject matter covered. It is sold on the understanding that the Publisher is not engaged in rendering professional services. If professional advice or other expert assistance is required, the services of a competent professional should be sought.

Anniversary Logo Design: Richard J. Pacifico

British Library Cataloguing in Publication Data

A catalogue record for this book is available from the British Library

ISBN 978-0-470-51020-9 (HB)

Typeset in 10/12 pt Times by Thomson Digital, India
Printed and bound in Great Britain by Antony Rowe Ltd, Chippenham, Wiltshire
This book is printed on acid-free paper responsibly manufactured from sustainable forestry in which at least two trees are planted for each one used for paper production.

Disclaimer: This book is not intended as a guide for vehicle modification, and anyone who uses it as such does so entirely at their own risk. Testing vehicle performance may be dangerous. The author and publisher are not liable for consequential damage arising from application of any information in this book.

Contents

Preface	xiii
Acknowledgements	xv
1 Introduction	1
1.1 History	1
1.2 Types of Friction	15
1.3 Damper Configurations	17
1.4 Ride-Levelling Dampers	33
1.5 Position-Dependent Dampers	35
1.6 General Form of the Telescopic Damper	37
1.7 Mountings	42
1.8 Operating Speeds and Strokes	47
1.9 Manufacture	53
1.10 Literature Review	54
2 Vibration Theory	61
2.1 Introduction	61
2.2 Free Vibration Undamped (1-dof)	61
2.3 Free Vibration Damped (1-dof)	63
2.4 Forced Vibration Undamped (1-dof)	68
2.5 Forced Vibration Damped (1-dof)	71
2.6 Coulomb Damping	74
2.7 Quadratic Damping	77
2.8 Series Stiffness	79
2.9 Free Vibration Undamped (2-dof)	85
2.10 Free Vibration Damped (2-dof)	85
2.11 The Resonant Absorber	86
2.12 Damper Models in Ride and Handling	87
2.13 End Frequencies	88
2.14 Heave and Pitch Undamped 1-dof	90
2.15 Heave and Pitch Damped 1-dof	91
2.16 Roll Vibration Undamped	93

2.17	Roll Vibration Damped	94
2.18	Heave-and-Pitch Undamped 2-dof	95
2.19	Heave-and-Pitch Damped 2-dof Simplified	100
2.20	Heave-and-Pitch Damped 2-dof Full Analysis	102
3	Ride and Handling	105
3.1	Introduction	105
3.2	Modelling the Road	105
3.3	Ride	111
3.4	Time-Domain Ride Analysis	113
3.5	Frequency-Domain Ride Analysis	117
3.6	Passenger on Seat	118
3.7	Wheel Hop	119
3.8	Handling	120
3.9	Axle Vibrations	122
3.10	Steering Vibrations	124
3.11	The Ride–Handling Compromise	124
3.12	Damper Optimisation	129
3.13	Damper Asymmetry	131
4	Installation	135
4.1	Introduction	135
4.2	Motion Ratio	135
4.3	Displacement Method	137
4.4	Velocity Diagrams	138
4.5	Computer Evaluation	138
4.6	Mechanical Displacement	138
4.7	Effect of Motion Ratio	139
4.8	Evaluation of Motion Ratio	142
4.9	The Rocker	142
4.10	The Rigid Arm	148
4.11	Double Wishbones	150
4.12	Struts	153
4.13	Pushrods and Pullrods	155
4.14	Motorcycle Front Suspensions	156
4.15	Motorcycle Rear Suspensions	160
4.16	Solid Axles	165
4.17	Dry Scissor Dampers	168
5	Fluid Mechanics	169
5.1	Introduction	169
5.2	Properties of Fluids	170
5.3	Chemical Properties	171
5.4	Density	171
5.5	Thermal Expansion	172

5.6	Compressibility	172
5.7	Viscosity	173
5.8	Thermal Capacity	175
5.9	Thermal Conductivity	176
5.10	Vapour Pressure	176
5.11	Gas Density	176
5.12	Gas Viscosity	177
5.13	Gas Compressibility	177
5.14	Gas Absorbability	177
5.15	Emulsification	179
5.16	Continuity	188
5.17	Bernoulli's Equation	188
5.18	Fluid Momentum	189
5.19	Pipe Flow	191
5.20	Velocity Profiles	196
5.21	Other Losses	199
5.22	The Orifice	203
5.23	Combined Orifices	207
5.24	Vortices	209
5.25	Bingham Flow	212
5.26	Liquid-Solid Suspensions	212
5.27	ER and MR Fluids	214
6	Valve Design	217
6.1	Introduction	217
6.2	Valve Types	219
6.3	Disc Valves	220
6.4	Rod Valves	221
6.5	Spool Valves	222
6.6	Shim Valves	223
6.7	Valve Characteristics	225
6.8	Basic Valve Models	227
6.9	Complete Valve Models	230
6.10	Solution of Valve Flow	235
6.11	Temperature Compensation	237
6.12	Position-Sensitive Valves	240
6.13	Acceleration-Sensitive Valves	240
6.14	Pressure-Rate Valves	243
6.15	Frequency-Sensitive Valves	245
6.16	Stroke-Sensitive Valves	245
6.17	Piezoelectric Valves	249
6.18	Double-Acting Shim Valves	249
6.19	Rotary Adjustables	250
6.20	Bellows Valves	252
6.21	Simple Tube Valves	252

6.22	Head Valves	257
6.23	Multi-Stage Valves	257
7	Damper Characteristics	259
7.1	Introduction	259
7.2	Basic Damper Parameters	263
7.3	Mechanical Friction	265
7.4	Static Forces	268
7.5	Piston Free Body Diagram	269
7.6	Valve Flow Rates	271
7.7	Pressures and Forces	272
7.8	Linear Valve Analysis	273
7.9	Cavitation	274
7.10	Temperature	276
7.11	Compressibility	276
7.12	Cyclical Characteristics, $F(X)$	278
7.13	Extreme Cyclic Operation	282
7.14	Stresses and Strains	283
7.15	Damper Jacking	286
7.16	Noise	287
8	Adjustables	289
8.1	Introduction	289
8.2	The Adjustable Valve	290
8.3	Parallel Hole	294
8.4	Series Hole	294
8.5	Maximum Area	294
8.6	Opening Pressure	294
8.7	Area Coefficient (Stiffness)	295
8.8	Automatic Systems	295
8.9	Fast Adaptive Systems	299
8.10	Motion Ratio	301
9	ER and MR Dampers	303
9.1	Introduction	303
9.2	ER–MR History	303
9.3	ER Materials	309
9.4	ER Dampers	314
9.5	ER Controlled Valve	319
9.6	MR Materials	321
9.7	MR Dampers	324
10	Specifying a Damper	333
10.1	Introduction	333

10.2	End Fittings	334
10.3	Length Range	334
10.4	$F(V)$ Curve	334
10.5	Configuration	334
10.6	Diameter	335
10.7	Oil Properties	335
10.8	Life	335
10.9	Cost	335
11	Testing	337
11.1	Introduction	337
11.2	Transient Testing	338
11.3	Electromechanical Testers	342
11.4	Hydraulic Testers	344
11.5	Instrumentation	345
11.6	Data Processing	346
11.7	Sinusoidal Test Theory	348
11.8	Test Procedure	352
11.9	Triangular Test	354
11.10	Other Laboratory Tests	356
11.11	On-Road Testing	357
	Appendix A: Nomenclature	361
	Appendix B: Properties of Air	375
	Appendix C: Properties of Water	379
	Appendix D: Test Sheets	381
	Appendix E: Solution of Algebraic Equations	385
	Appendix F: Units	393
	Appendix G: Bingham Flow	397
	References	401
	Index	409

Preface to Second Edition

In view of the tremendous worldwide production of automotive dampers (shock absorbers), the former absence of a book devoted to this topic is surprising. During some years of damper design, research and commercial testing, the author has become aware of a need for a suitable book to present the fundamentals of damper design and use, for the benefit of the many designers of vehicles such as passenger cars, motorcycles, trucks, racing cars and so on, since the necessary body of knowledge is far from readily available in the research literature. Damper designers themselves will already be familiar with most of the material here, but may find some useful items, especially with regard to installation motion ratios and behaviour of the vehicle as a whole, but in any case will probably be pleased to see the basic material collected together.

As in my previous work, I have tried to present the basic core of theory and practice, so that the book will be of lasting value. I would be delighted to hear from readers who wish to suggest any improvements to presentation or coverage.

Amongst many suggestions received for additions and improvements to the first edition, there was clearly a desire that the book should be extended to cover extensively the effect of the damper on ride and handling. The extra material would, however, be vast in scope, and would greatly increase the size and expense of the book. Also, in the author's view, such analysis belongs in a separate book on ride quality and handling, where the effect of the damper can be considered fully in the context of other suspension factors.

Instead, the general character of the first edition has been retained, with its emphasis on the internal design of the damper. Considerable efforts have been made to eliminate known errors in the first edition, and substantial detailed additions and revisions have been made. In many areas the material has been reorganised for greater clarity. The variety of damper types found historically is now more fully covered, and the recent developments in magnetorheological dampers are now included. Conventional damper valve design is considered much more carefully, and more space is allocated to detailed variations in valve design, including stroke-sensitive types. Many new figures have been added. On this basis, it is hoped that the new edition will offer a worthwhile service to the vehicle design community, at least as an introduction to the complex and fascinating field of damper design.

Finally, the title *The Shock Absorber Handbook* has been controversial, as it was said that the subject was not shock absorbers and it was not a handbook. It would probably have been better to use the technically correct term *damper*, with a title such as *The Automotive Damper*. However, a change of title has been deemed impractical given that the book is well established under its original name, and it has been decided to remain with the devil that we know for this, second, edition.

John C. Dixon

Acknowledgements

Numerous figures are reproduced by permission of the Society of Automotive Engineers, The Institution of Mechanical Engineers, and others. The reference for all previously published figures is given with the figure.

1

Introduction

1.1 History

The current world-wide production of vehicle dampers, or so-called shock absorbers, is difficult to estimate with accuracy, but is probably around 50–100 million units per annum with a retail value well in excess of one billion dollars per annum. A typical European country has a demand for over 5 million units per year on new cars and over 1 million replacement units, The US market is several times that. If all is well, these suspension dampers do their work quietly and without fuss. Like punctuation or acting, dampers are at their best when they are not noticed - drivers and passengers simply want the dampers to be trouble free. In contrast, for the designer they are a constant interest and challenge. For the suspension engineer there is some satisfaction in creating a good new damper for a racing car or rally car and perhaps making some contribution to competition success. Less exciting, but economically more important, there is also satisfaction in seeing everyday vehicles travelling safely with comfortable occupants at speeds that would, even on good roads, be quite impractical without an effective suspension system.

The need for dampers arises because of the roll and pitch associated with vehicle manoeuvring, and from the roughness of roads. In the mid nineteenth century, road quality was generally very poor. The better horse-drawn carriages of the period therefore had soft suspension, achieved by using long bent leaf springs called semi-elliptics, or even by using a pair of such curved leaf springs set back-to-back on each side, forming full-elliptic suspension. No special devices were fitted to provide damping; rather this depended upon inherent friction, mainly between the leaves of the beam springs. Such a set-up was appropriate to the period, being easy to manufacture, and probably worked tolerably well at moderate speed, although running at high speed must have been at least exciting, and probably dangerous, because of the lack of damping control.

The arrival of the so-called horseless carriage, i.e. the carriage driven by an internal combustion engine, at the end of the nineteenth century, provided a new stimulus for suspension development which continues to this day. The rapidly increasing power available from the internal combustion engine made higher speeds routine; this, plus the technical aptitude of the vehicle and component designers, coupled with a general commercial mood favouring development and change, provided an environment that led to invention and innovation.

The fitting of damping devices to vehicle suspensions followed rapidly on the heels of the arrival of the motor car itself. Since those early days the damper has passed through a century of evolution, the basic stages of which may perhaps be considered as:

- (1) dry friction (snubbers);
- (2) blow-off hydraulics;
- (3) progressive hydraulics;
- (4) adjustables (manual alteration);
- (5) slow adaptives (automatic alteration);
- (6) fast adaptives ('semi-active');
- (7) electrofluidic, e.g. magnetorheological.

Historically, the zeitgeist regarding dampers has changed considerably over the years, in roughly the following periods:

- (1) Up to 1910 dampers were hardly used at all. In 1913, Rolls Royce actually discontinued rear dampers on the Silver Ghost, illustrating just how different the situation was in the early years.
- (2) From 1910 to 1925 mostly dry snubbers were used.
- (3) From 1925 to 1980 there was a long period of dominance by simple hydraulics, initially simply constant-force blow-off, then through progressive development to a more proportional characteristic, then adjustables, leading to a mature modern product.
- (4) From 1980 to 1985 there was excitement about the possibilities for active suspension, which could effectively eliminate the ordinary damper, but little has come of this commercially in practice so far because of the cost.
- (5) From 1985 it became increasingly apparent that a good deal of the benefit of active suspension could be obtained much more cheaply by fast auto-adjusting dampers, and the damper suddenly became an interesting, developing, component again.
- (6) From about 2000, the introduction, on high-price vehicles at least, of controllable magnetorheological dampers.

Development of the adaptive damper has occurred rapidly. Although there will continue to be differences between commercial units, such systems are now effective and can be considered to be mature products. Fully active suspension offers some performance advantages, but is not very cost effective for passenger cars. Further developments can then be expected to be restricted to rather slow detail refinement of design, control strategies and production costs. Fast acting control, requiring extra sensors and controls, will continue to be more expensive, so simple fixed dampers, adjustables and slow adaptive types will probably continue to dominate the market numerically for the foreseeable future.

The basic suspension using the simple spring and damper is not ideal, but it is good enough for most purposes. For low-cost vehicles, it is the most cost-effective system. Therefore much emphasis remains on improvement of operating life, reliability and low-cost production rather than on refinement of performance by technical development. The variable damper, in several forms, has now found quite wide application on mid-range and expensive vehicles. On the most expensive passenger and sports cars, magnetorheologically controlled dampers are now a popular fitment, at significant expense.

The damper is commonly known as the shock absorber, although the implication that shocks are absorbed is misleading. Arguably, the shocks are 'absorbed' by the deflection of the tires and springs. The purpose of dampers is to dissipate any energy in the vertical motion of body or wheels, such motion having arisen from control inputs, or from disturbance by rough roads or wind. Here 'vertical' motion includes body heave, pitch and roll, and wheel hop. As an agglomeration of masses and springs, the car with its wheels constitutes a vibrating system that needs dampers to optimise control behaviour, by preventing response overshoots, and to minimise the influence of some unavoidable resonances. The mathematical theory of vibrating systems largely uses the concept of a linear damper, with force proportional to extension speed, mainly because it gives equations for which the solutions are well understood and documented, and usually tolerably realistic. There is no obligation on a damper to exhibit such a characteristic; nevertheless the typical modern hydraulic damper does so approximately. This is because the vehicle and damper manufacturers consider this to be desirable for good physical

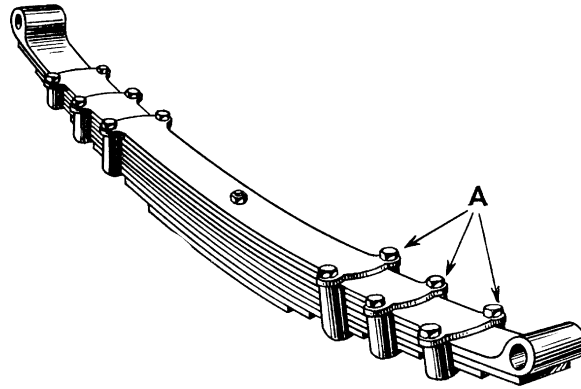


Figure 1.1.1 Dry friction damping by controlled clamping (adjustable normal force) of the leaf spring (Woodhead).

behaviour, not for the convenience of the theorist. The desired characteristics are achieved only by some effort from the manufacturer in the detail design of the valves.

Damper types, which are explained fully later, can be initially classified as

- (a) dry friction with solid elements;
 - (i) scissor;
 - (ii) snubber;
- (b) hydraulic with fluid elements;
 - (i) lever-arm;
 - (ii) telescopic.

Only the hydraulic type is in use in modern times. The friction type came originally as sliding discs operated by two arms, with a scissor action, and later as a belt wrapped around blocks, the ‘snubber’. The basic hydraulic varieties are lever-arm and telescopic. The lever-arm type uses a lever to operate a vane, now extinct, or a pair of pistons. Telescopic, now most common, are either double-tube or gas-pressurised single-tube.

The early days of car suspension gave real opportunities for technical improvement, and financial reward. The earliest suspensions used leaf springs with inherent interleaf friction. Efforts had been made to control this to desirable levels by the free curvature of the leaves. Further developments of the leaf spring intrinsic damping included controlled adjustment of the interleaf normal forces, Figure 1.1.1, and the use of inserts of various materials to control the friction coefficients, Figure 1.1.2.

Truffault invented the scissor-action friction disc system before 1900, using bronze discs alternating with oiled leather, pressed together by conical disc springs and operated by two arms, with a floating body. The amount of friction could be adjusted by a compression hand-screw, pressing the discs together more or less firmly, varying the normal force at approximately constant friction coefficient. Between 1900 and 1903, Truffault went on to develop a version for cars, at the instigation

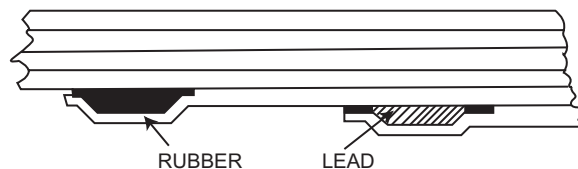


Figure 1.1.2 Leaf spring inserts to control the friction coefficient and consequent damping effect.

GREATEST SPEED EVER ATTAINED IN HISTORY OF THE WORLD

At Brescia, Italy, on Sept. 4th, Lancia, with his 80 H. P. Fiat won the Italian road race, beating the most renowned racing cars of Europe.

230 Miles in 3 Hours 10 Minutes 56 Seconds

Making the unheard-of long distance average of 72 MILES AN HOUR, beating all railroad records. This was only possible by use of the famous

Truffault-Hartford Suspension



RECENT VICTORIES

French Eliminating trials, They—"Richard-Brasier," 80 H. P.) Beat nearest competitor 25 mins.

Gordon-Bennett Cup (They—"Richard-Brasier," 80 H. P.) Wrested cup from Germany and the famous Mercedes.

Mile Standing Start (Baras—"Darracq" 80 H. P.) World record lowered 5 secs.

Flying Kilometre (Rigolly—"Gobron Brillie"). 104 miles an hour.

Harry Harkness, Long Branch, Aug. 17, (60 H. P. "Mercedes"). Cut the world 50 mile track record 16 mins. 27 secs.

Providence, Sept. 10, (H. L. Bowden—90 H. P. "Mercedes"). 2-10 mile track records lowered.

"Diminishes in a remarkable degree the wear on the tires."—*Michelin*.

"Was able to drive at highest speed over all obstructions."—*They*.

"Remarkable and perfect suspension."—*Mercedes Co.*

Although indispensable for racing cars, its greatest utility is for ordinary touring cars or runabouts.

Are you not tired of being jolted and jarred?

Can be applied to any car in a few hours.

Address E. V. HARTFORD, 67 Vestry St., New York City

Telephone, 3754 Spring

Figure 1.1.3 An advertisement from 1904 for the early Truffault designed dry friction scissor damper manufactured by Hartford.

of Hartford in the US, who began quantity production in 1904, as in Figures 1.1.3–1.1.5. Truffault, well aware of the commercial potential, also licensed several other manufacturers in Europe, including Mors and Peugeot in France, who also had them in production and use by 1904. A similar type of damper was also pressed into service on the steering, Figure 1.1.6, to reduce steering fight on rough roads and to reduce steering vibrations then emerging at higher speeds and not yet adequately understood.

Figure 1.1.7 shows an exploded diagram of a more recent (1950s) implementation from a motorcycle. This is also adjustable by the hand-screw. Subsequent to the Truffault–Hartford type, The Hartford Telecontrol (the prefix *tele* means remote) developed the theme, Figure 1.1.8, with a convenient Bowden cable adjustment usable by the driver *in situ*. A later alternative version, the Andre Telecontrol, had dry friction scissor dampers, but used hydraulic control of the compression force and hence of the damper friction moment.

In 1915, Claud Foster invented the dry friction block-and-belt snubber, Figure 1.1.9, manufactured in very large quantities by his Gabriel company, and hence usually known as the Gabriel Snubber. In view of the modern preference for hydraulics, the great success of the belt snubber was presumably based on low cost, ease of retrofitment and reliability rather than exceptional performance.

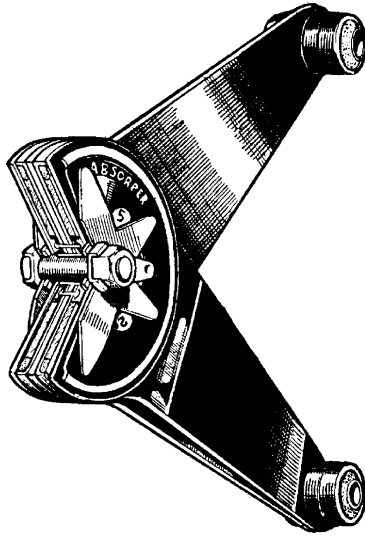


Figure 1.1.4 The Andre-Hartford scissor-action dry friction damper.

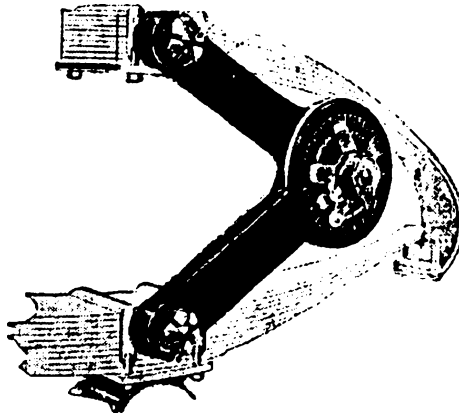
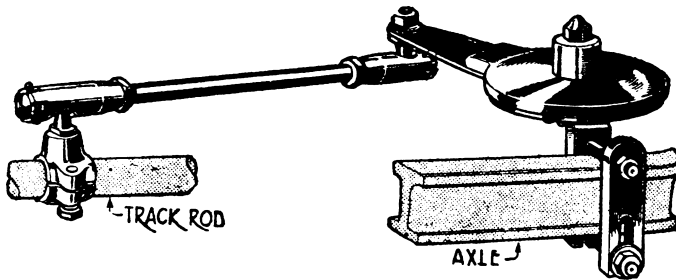


Figure 1.1.5 Installation of a dry-friction scissor damper on three-quarter-elliptic leaf springs (from Simanaitis, 1976).



A Damping Device for Preventing Wheel Wobble on Rigid-Type Front Axles.

Figure 1.1.6 Use of the Truffault-Hartford rotary dry friction damper on steering.

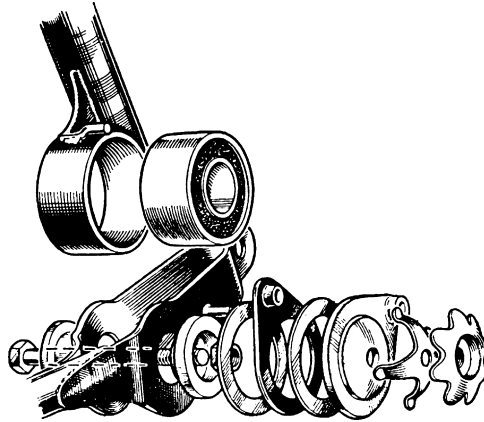


Figure 1.1.7 The Greeves motorcycle front suspension from around 1950 had a rubber-in-torsion spring, using an integral rotary dry friction damper easily adjustable by hand.

The spring-loaded blocks are mounted on the body, in particular on the chassis rails in those days, with the leather belt being fixed to the wheel upright or axle. In upward motion of the suspension, the snubber has no effect, but the spring-loaded blocks take up any slack. Any attempt by the suspension to extend will be opposed by the belt which has considerable friction where it wraps over itself and around the blocks. Hence the action is fully asymmetrical. The actual performance parameters do not seem to have been published. Some theoretical analysis may be possible, derived from the standard theory of wrapped circular members, with friction force growing exponentially with wrapping angle, for prediction of the force in relation to block shape, spring force and stiffness and belt-on-belt and belt-on-block coefficients of friction. The overall characteristic, however, seems to be an essentially velocity-independent force in extension, i.e. fully asymmetrical Coulomb damping. The characteristics could have been affected in service conditions by the friction-breaking effect of engine vibrations.

An early form of hydraulic contribution to damping was the Andrex oil-bath damper, Figure 1.1.10. This had metal and leather discs as in the dry damper, but was immersed in a sealed oil bath. There may also have been a version with separated metal discs relying on oil in shear. Another version, Figure 1.1.11, was adjustable from the dashboard, with oil pressure transmitted to the dampers to control the normal force on the discs, or perhaps in some cases to adjust the level of oil in the case. The pressure gauge in Figure 1.1.11 suggests that this type was controlling the normal force.

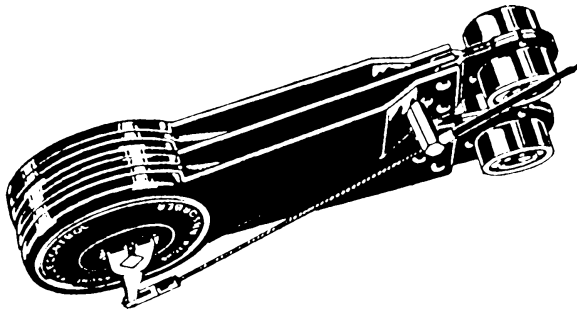


Figure 1.1.8 The Hartford Telecontrol damper was adjustable via a Bowden cable, and hence could be controlled easily from the driving seat, even with the vehicle in motion.

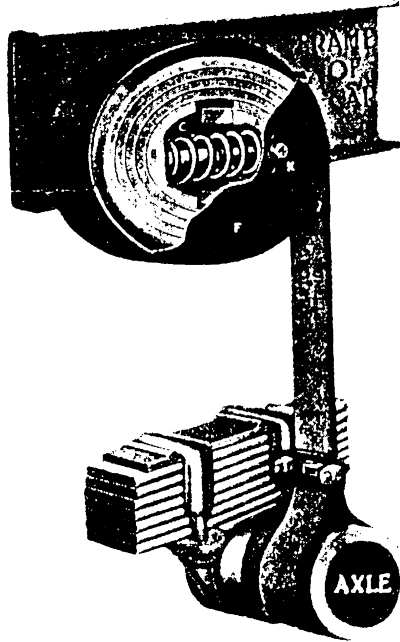


Figure 1.1.9 The Gabriel Snubber (1915) used a leather strap around sprung metal or wooden blocks to give restraint in rebound only (from Simanaitis, 1976).

The early development timetable of dampers thus ran roughly as follows:

- 1901: Horock patents a telescopic hydraulic unit, laying the foundations of the modern type.
- 1902: Mors actually builds a vehicle with simple hydraulic pot dampers.
- 1905: Renault patents an opposed piston hydraulic type, and also patents improvements to Horock's telescopic, establishing substantially the design used today.
- 1906: Renault uses the piston type on his Grand Prix racing cars, but not on his production cars. Houdaille starts to develop his vane-type.
- 1907: Caille proposes the single-lever parallel-piston variety.

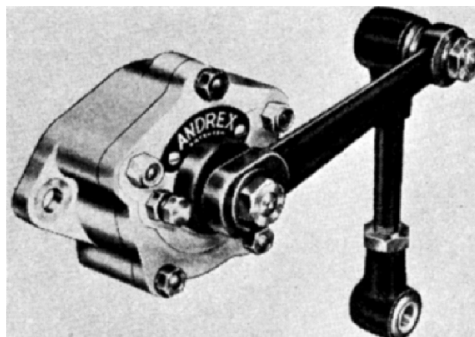


Figure 1.1.10 The Andrex multiple discs-in-oil-bath damper.

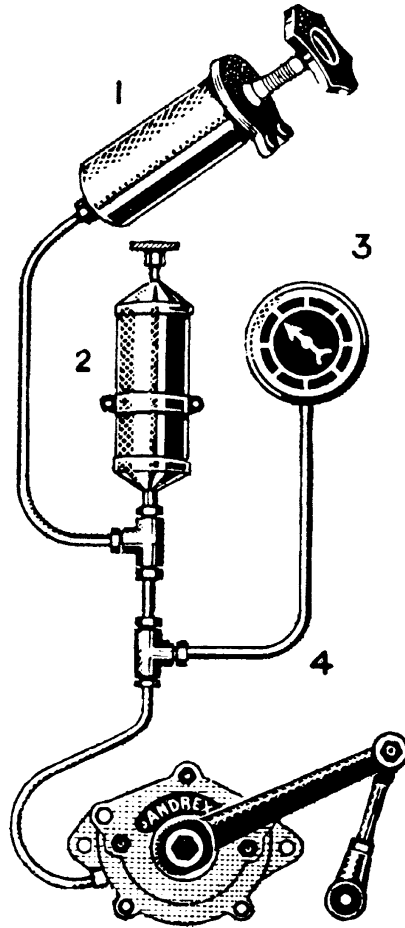


Figure 1.1.11 The adjustable version of the Andrex oil-bath damper included pump, reservoir and pressure gauge.

1909: A single-acting Houdaille vane type is fitted as original equipment, but this is an isolated success for the hydraulic type, the friction disc type remaining dominant.

1910: Oil damped undercarriages come into use on aircraft.

1915: Foster invents the belt 'snubber' which had great commercial success in the USA.

1919: Lovejoy lever-arm hydraulic produced in the USA.

1924: Lancia introduces the double-acting hydraulic unit, incorporated in the front independent pillar suspension of the Lambda. The Grand Prix Bugatti uses preloaded nonadjustable drum-brake type.

1928: Hydraulic dampers are first supplied as standard equipment in the USA.

1930: Armstrong patents the telescopic type.

1933: Cadillac 'Ride Regulator' driver-adjustable five-position on dashboard.

1934: Monroe begins manufacture of telescopics.

1947: Koning introduces the adjustable telescopic.

1950: Gas-pressurised single-tube telescopic is invented and manufactured by de Carbon.

2001: Magnetorheological high-speed adjustables introduced (Bentley, Cadillac).

The modern success of hydraulics over dry friction is due to a combination of factors, including:

- (1) Superior performance of hydraulics, due to the detrimental effect of dry Coulomb friction which is especially noticeable on modern smooth roads.
- (2) Damper life has been improved by better seals and higher quality finish on wearing surfaces.
- (3) Performance is now generally more consistent because of better quality control.
- (4) Cost is less critical than of old, and is in any case controlled by mass production on modern machine tools.

During the 1950s, telescopic dampers gradually became more and more widely used on passenger cars, the transition being essentially complete by the late 1950s. In racing, at Indianapolis the hydraulic vane type arrived in the late 1920s, and was considered a great step forward; the adjustable piston hydraulic appeared in the early 1930s, but the telescopic was not used there until 1950. Racing cars in Europe were quite slow to change, although the very successful Mercedes Benz racers of 1954–55 used telescopics. Although other types are occasionally used, the telescopic hydraulic type of damper is now the widely accepted norm for cars and motorcycles.

It was far from obvious in early days that the hydraulic type of damper would ultimately triumph, especially in competition with the very cost-effective Gabriel snubber of 1915. The first large commercial successes for the hydraulic types came with the vane-type, developed from 1906 onwards by Maurice Houdaille. The early type used two arms with a floating body, a little like the dry friction scissor damper. The later type still used vanes, but had a body mounted on the vehicle sprung mass, operated by an arm with a drop link to the leaf spring suspension, Figures 1.1.12–1.1.14.

The 1919 Motor Manual (UK, 21st edition) devoted less than one of its three hundred pages to dampers, suggesting that the damper was not really considered to be of great importance in those days, stating that:

These devices, of which there are a great number on the market, are made for the purpose of improving the comfortable running of the car, more especially on roughly-surfaced roads. The present system of springing is

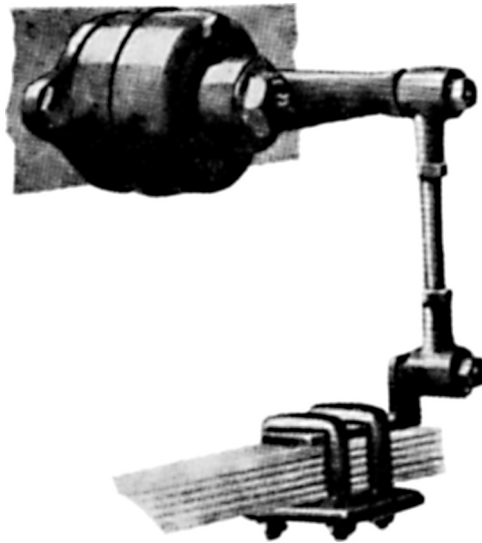


Figure 1.1.12 The Houdaille rotary vane damper, the first large quantity production hydraulic damper. This originated in 1909 and was double-acting from 1921.

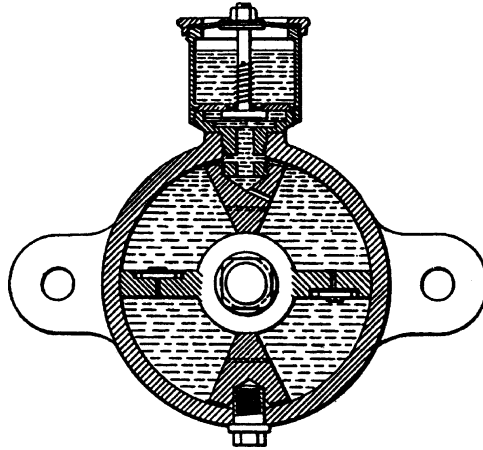


Figure 1.1.13 Cross-section of slightly different version of Houdaille rotary vane damper (from Simanaitis, 1976).

admittedly not perfect, and when travelling on rough roads there is the objectionable rebound of the body after it passes over a depression in the road, which it is desirable should be reduced as much as possible. The shock from this rebound is not only uncomfortable for the passengers, but it has a bad effect on the whole car. Hence these shock absorbers are applied as the best means available so far to check the rebound. They are made on various principles, generally employing a frictional effect such as is obtainable from two hardened steel surfaces in close contact. Another principle is that of using the fluid friction of oil, practically on the lines of any of the well-known dash-pot devices, viz., a piston moving in a cylinder against the resistance offered by the oil contained within it, the oil passing slowly through a small aperture into another chamber. This type of device is probably the best solution of the problem.

Up to 1920 hydraulic dampers were single acting, in droop only, but from 1921 a more complex valve system allowed some damping in bump too. At this point the operating characteristics of the

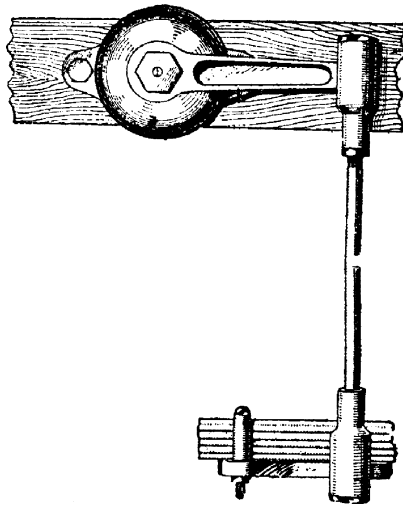


Figure 1.1.14 An early configuration of hydraulic damper, a rotary vane device with a drop arm to the axle. Note the wooden chassis rail (artist's impression, *The Motor Manual*, 1919).

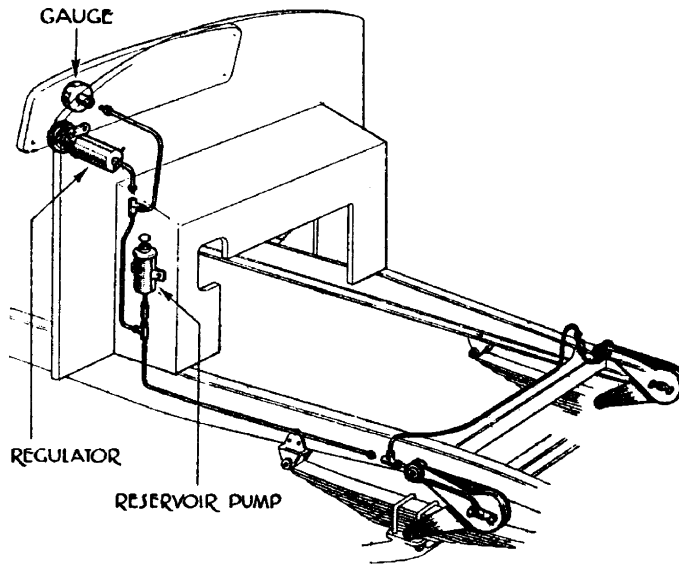


Figure 1.1.15 Layout of the hydraulically remote Andre Telecontrol damper, shown here on a front axle (The Motor Manual, 1939).

hydraulic damper had largely reached their modern form. More recent developments have had more to do with the general configuration, so that the lever-operated type has given way to the telescopic piston type which is cost-effective in manufacture, being less critical with regard to seal leakage, and has better air cooling, although lacking the conduction cooling of a body-mounted lever-arm damper. Most importantly perhaps, the telescopic type lends itself well to the modern form of suspension in terms of its mounting and ease of installation.

The 1939 Motor Manual (UK, 30th edition), devoted three pages to dampers, perhaps indicating the increased recognition of their importance for normal vehicles. An illustration was included of the Andre-Hartford dry friction scissor, and also one of the Luvax vane damper, shown later. There was also a diagram of the hydraulically adjusted, but dry action, version of the Andre Telecontrol system, as seen in Figure 1.1.15. That writer was moved to offer some additional explanation of damping and ‘shock absorbing’ in general, stating that:

Whatever form of springing is employed, it is always considered necessary to damp the suspension by auxiliaries, which have become known as shock absorbers. This term is unfortunate, because it is the function of the springs to absorb shocks, whereas the ‘shock absorbers’ serve the purpose of providing friction in a controlled form which prevents prolonged bouncing or pitching motions, by absorbing energy. A leaf spring is inherently damped by the friction between the leaves, and it may, therefore, seem strange that after lubricating these leaves friction should be put back into the system by the use of shock absorbers. The explanation is that leaf friction is not readily controllable, whereas the shock absorber imparts a definite and adjustable degree of damping to the system.

The most popular type of shock absorber is an hydraulic device which is bolted to the frame and is operated by an arm coupled to the axle. Four such devices are ordinarily fitted. When relative movement occurs between the axle and the frame, the arm on the shock absorber spindle is oscillated, and this motion is conveyed to a rotor, which fits within a circular casing. Oil in the casing is made to flow through valves from one side of the rotor to the other and so creates hydraulic resistance which damps the oscillations. In some cases the valves are arranged to give ‘double action’, the damping then being effective on both deflection and rebound. In other cases single-acting devices are used which can check rebound only. As a rule the action of the shock absorbers can be adjusted by means of a screw, which alters the tension of a spring and so varies the load on a ball valve.

The hydraulic shock absorber has the important merit of increasing its damping effect when subject to sudden movements, but suffers from the defect of providing very little resistance against slower motions, such as rolling. Consequently, for sports cars many users prefer frictional shock absorbers, of the scissor (constant resistance) type, of which the most famous is the Andre–Hartford.

The final comment above is significant in a modern context, regarding the preferred velocity–force relationship, which is a regressive shape with a ‘knee’, rather than simply linear.

The Lancia Lambda of 1925 had sliding pillar suspension, Figure 1.1.16, now almost extinct (except, e.g. Morgan) and regarded as primitive, but highly successful at the time. It was noted for the fact that its oil-filled cylinders required no maintenance, and was very reliable. This is an attractive option for a light vehicle, because it is such a compact and light system, although lacking the ability of modern suspensions to be adjusted to desired handling characteristics by detailed changes to the geometry.

Although dry friction snubbers remained in wide use through to the 1930s, hydraulic fluid-based dampers were in limited use from very early days and continued to grow in popularity. An early successful version in the USA was made by Lovejoy, Figure 1.1.17.

Difficulties with sealing and wear of vane lever arm types led to the lever arm parallel piston system as in the Lovejoy and in the Armstrong, Figure 1.1.18, in which the valve may also easily be made

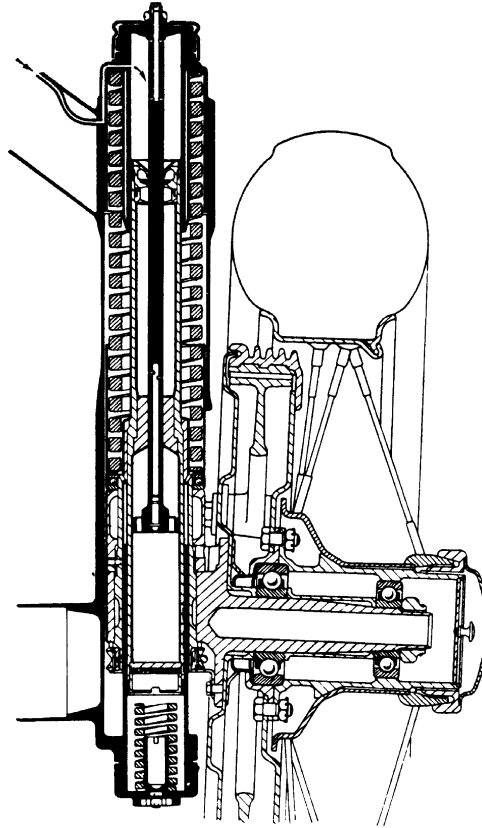


Figure 1.1.16 The Lancia Lambda sliding-pillar system had the spring and damper sealed into one unit (Lancia, 1925).